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# Renewable and Sustainable Energy Reviews





# Aluminum as energy carrier: Feasibility analysis and current technologies overview

E.I. Shkolnikov, A.Z. Zhuk, M.S. Vlaskin\*

The Joint Institute for High Temperatures, Ijorskaya st. 13/2, 125412, Moscow, Russia

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#### ABSTRACT

Aluminum is examined as energy storage and carrier. To provide the correct feasibility study the work includes the analysis of aluminum production process: from ore to metal. During this analysis the material and energy balances are considered. Total efficiency of aluminum-based energy storage is evaluated.

Aluminum based energy generation technologies are reviewed. Technologies are categorized by aluminum oxidation method. Particularly, the work focuses on direct electrochemical (anodic) oxidation of aluminum, aluminum—water reaction in alkaline solution, mechanochemical activation of aluminum, mechanical activation of aluminum and high-temperature aluminum—water reaction. The objective is methods overview including technological principle, efficiency, urgent problems and possible application areas.

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<sup>\*</sup> Corresponding author. Tel.: +7 495 4851055; fax: +7 495 4851055. E-mail address: vlaskin@inbox.ru (M.S. Vlaskin).

#### 1. Looking for an appropriate energy carrier

#### 1.1. Need for energy storage technologies

A number of independent institutions predict that the oil, today's basic fuel in transport and small stationary energy, in near future will peak and its production will go into decline [1–6]. One of the world energy scenarios supposes that oil production would not exceed 90 million barrel/day and decline will start before 2020 [7]. Oil production reduction is going to be provided not only by oil reserves depletion but also due to efforts in alternative energy. It is predicted that renewable-based electricity generation will triple between 2008 and 2035 and increase in global generation from 19% in 2008 to almost one-third in 2035 [7]. At the same time the backbone of global energy in the next decades will remain the coal and word's base electricity load will be attached to large and remote coal-fired units. To remove the oil from transport, to support the renewable, distributed and Smart-grid energy and to smooth the load of centralized coal-fired and nuclear power plants, the energy storage technologies are required. To sum up, oil problems, efforts in renewables and coal predominance, as well as continued human industrialization and informatization all together need to store the

Energy storages are urgently needed at all energy scales: from portable and transport to large stationary. Different applications can make significantly various demands, thus diversifying the spectrum of energy storage technologies. Today the variety of energy storage includes the following: batteries (lead-acid [8-11], sodium sulphur [12], Ni-based [13,14], Li-based [15-18], flow batteries [19-21], etc.), supercapacitors [22], superconducting magnetic energy storage [23], flywheel storage [24,25], pumped hydro storage [26], pneumatic storage [27-29] and others. Energy storage technologies have been already reviewed and compared [30-37]. The summary of recent reviews is presented in Table 1. Although there are a great number of commercially available energy storage technologies, none of above listed systems can be referred to as universal and each has its own specialized application areas. Sodium sulphur battery, vanadium redox flow battery, pumped hydro storage and compressed air energy storage are only stationary. Most technologies return the energy back to the grid. Only conventional batteries such as lead-acid, nickel cadmium and lithium ion are supposed to carry the energy. Batteries have high electrical efficiency, rapid response and relatively low self-discharge, but suffer from low energy density and short lifetime. Last disadvantages prevent the batteries from large-scale (over 50 MWh per unit) energy storage applications. Moreover, if the capacity of conventional batteries increases, there will be a problem of the natural abundance of used metals [33,38]. Therefore, there are still no sustainable alternatives for energy carrying and the replacement of oil from its traditional niches by energy storage technologies seems to be far from reality.

#### 1.2. Perspective inorganic energy carriers

High-level integration like with liquid hydrocarbons within global energy is possible only in case of energy carriers based on the most widespread chemical elements in the earth's crust or lithosphere. In simple case the energy can be stored in the form of chemical energy of reduced inorganic substances such as hydrogen [39,40], silicon [41], aluminum [42], iron [43], magnesium [44] and others. The process of energy accumulation occurs when the substance is produced from respective oxide. The energy is then regenerated, when the substance is oxidized. Such energy carriers differ from the conventional energy storage technologies because they represent the renewable synthetic fuels. They can be stored for a long time with negligible self-discharge and easily transported to any distance like fossil fuels.

Hydrogen has been already recognized to be one of perspective future energy carries. It can be produced from water through electrolysis that means that the potential reserve of hydrogen on the Earth is practically unlimited. Hydrogen is proposed to be used as a fuel in portable [45] and transport [46] and as energy storage in renewable and conventional power plants [30,32,33]. Especially, hydrogen production is bound up with nuclear reactors because of benefits of high temperature electrolysis [47–50]. Although hydrogen-based energy storage system has relatively low cycle efficiency, about 35% [32] (due to the combination of electrolytic cell and combustion cell), the hydrogen is much attractive energy carrier, because, theoretically, it has high energy density, can be used to store large amounts of energy and can be transported for a long distance (to remote non-electrified areas). Moreover, hydrogen is environmentally friendly in terms of that the process of its combustion is less polluting than that of fossil fuels, so the use of hydrogen for energy production decreases the charges for eco-activity. However, in spite of the fact that hydrogen energy has been under research for several decades up to now and for this time it has changed into individual scientific area [51], the hydrogen still has not obtained the recognition of energy market mainly due to storage and transportation problems [46,52], which are still open as decades ago.

While hydrogen is stopping, the attention falls on other energy carriers. To compete with hydrogen and oil in basic fields the alternative inorganic energy carrier must first of all be composed of the most widespread substances like those presented in Table 2. The use of presented substances in synthetic fuel production should expand the spectrum of suitable minerals and so decrease the fuel cost. There is a dream to use ordinary sand as raw for synthetic fuel [41,53]. However, an appropriate fuel composition must be formed in accordance with both production process and oxidation technology efficiencies. Generally speaking, there is a wide spectrum of differently composed inorganic synthetic fuels, which might be used for energy storage and carrying, especially in post-fossil fuel era; the time will show which one will get the sustainability.

#### 1.3. Reasons for aluminum

Present work will be focused on aluminum. Unlike hydrogen, aluminum is easy to transport and store. When metal is placed into the atmosphere, it is covered by oxide film, which protects metal from further corrosion [54], thus providing the safety of its storage and transportation. Like hydrogen, aluminum is renewable. It has high calorific value, high concentration in the earth's crust [55,56] and high current production level [57–59]. So, aluminum can be regarded as perspective energy carrier and has a good chance for large-scale integration in global energy storage.

To provide the correct feasibility study this work will be started from aluminum production process analysis, which will examine the whole chain: from ore to metal. During this analysis the material and energy balance will be considered.

Then, the technologies, which use aluminum as fuel or energy source, will be reviewed. Technologies differ from each other manly by aluminum oxidation method. When aluminum is oxidized the oxide film, which provides the safety of aluminum storage and transportation, creates an obstacle to efficient utilization of aluminum within power plants. To increase the efficiency of aluminum-based energy generation technology the special actions such as alloying with certain elements, chemical activators addition, mechanical or mechanochemical treatment, heating and other are applied. The objective of this work is such methods overview including technological principle, efficiency, urgent problems and possible application areas.

**Table 1**Comparison of energy storage technologies.

Energy storage technology	Capacity range	Typical self-discharge	Cycle efficiency, %	Energy density, Wh/kg	Power density, W/kg	Lifetime	Application areas	
Lead-acid battery	1 W-10 MW	2%/month	70–90	30-50	100–200	1200–1800 cycles	Portable, electric/hybrid electric vehicle, small stationary	
Nickel cadmium battery	1 W-40 MW	10%/month	60-83	50-75	150–300	1500–3000 cycles	Portable, small stationary	
Nickel metal hydride battery	1 W-100 kW	30%/month	65–70	50-80	200-600	1500–3000 cycles	Portable, electric/hybrid electric vehicle	
Sodium nickel chloride	1 W-300 kW	15%/day	70–80	100–120	150-200	2500 cycles	Portable, hybrid electric vehicle	
Sodium sulphur battery	50 kW-34 MW	20%/day	75–92	150–240	150–230	2500–4500 cycles	Large stationary, power quality	
Lithium ion battery	1 W-100 kW	5%/month	85–100	100–200	150–300	1000–10,000 cycles	Portable, electric/hybrid electric vehicle, small stationary	
Lithium polymer battery	1 W-100 kW	5%/month	85–100	150	150-250	300-600 cycles	Portable, electric/hybrid electric vehicle, small stationary	
Vanadium redox flow battery	50 kW-250 kW	Small	75–85	10–30		>13,000 cycles	Small stationary	
Supercapacitor	1 W-300 kW	5%/day	85-98	0.5-5	>10,000	>500,000 cycles	Portable, hybrid electric vehicle, power quality	
Superconducting magnetic energy storage	1 MW-100 MW	10%/day	97–100	0.5–5	500-2000	>100,000 cycles	Power quality	
Flywheel storage	100 kW-250 kW	20%/h	90-95	5–100	>1000	20 years	Small stationary, power quality	
Pumped hydro storage	1 MW-5000 MW	Small	70-85	0.5-1.5		60 years	Large stationary	
Compressed air energy storage	50 MW-300 MW	Small	50–89	30-60		40 years	Large stationary	

**Table 2** Characteristics of energy storage matters.

Substance	Content in lithosphere, wt.%	Density, g/cm <sup>3</sup>	Calorific value, MJ/kg	Heat generation in water oxidation reaction, MJ/kg	Mass of $H_2$ produced in water oxidation reaction per a kg of substance, kg
Si	27.72	2.42	30.74	10.24	0.143
Al	8.13	2.7	30.97	15.03	0.111
Fe	5	7.87	7.35	-0.33	0.054
Ca	3.63	1.55	15.91	8.74	0.050
Na	2.83	1	9.05	2.82	0.043
Mg	2.09	1.74	25.11	13.16	0.083

# 2. Aluminum production process analysis

#### 2.1. Geology

Aluminum is one of the most widespread chemical elements in the outer 16 km of the crust (about 8% by weight [60,61]); only oxygen and silicon are more widespread, while among metals aluminum takes first place. The earth's crust contains aluminum mainly in the form of aluminum silicates.

The main raw for aluminum production is crystalline aluminum oxide – alumina ( $Al_2O_3$ ). Although alumina is contained within a great number of natural minerals, about 98% of metallurgical alumina is produced only from bauxite. Bauxite is a compound rock, which is composed of hydrous alumina (aluminum hydroxides and oxyhydroxides). There are also various compounds in bauxite such as iron oxide, silicon oxide, titanium dioxide and smaller amounts of other oxides. Bauxite contains 50–80% of hydrous alumina. The percentage of alumina varies from 30% to 60%. The composition of bauxite mined differs depending on mining location [62–66].

Table 3 shows bauxite composition suitable for metallurgical alumina production. Bauxite resources are estimated to be 55–75 billion tons [56] that is 275–375 times more than current annual rate of its extraction (about 200 million tons [56,67]).

# 2.2. Alumina refining

Of all bauxite mined, approximately 85% is used for metallurgical alumina production [68]. Alumina is extracted from bauxite by

**Table 3**Composition of bauxite suited for metallurgical alumina production.

Compound	Content, wt.%
Al <sub>2</sub> O <sub>3</sub> , min SiO <sub>2</sub> , max	30 20
Fe <sub>2</sub> O <sub>3</sub> , max	30
TiO <sub>2</sub> , max	6
other, max	1

**Table 4** Components of alumina prime cost.

Item	%	
Total	100	
Bauxite	24	
Auxiliary raw	9	
Energy	24	
Investment	26	
Wage cost & repair bill	17	

Bayer process. The chemistry of this process can be simplified by the following equation:

$$Al_2O_3 \cdot nH_2O + 2NaOH \rightleftharpoons 2NaAlO_2 + (n+1)H_2O$$
 (1)

Bayer process is usually considered in four stages [69]. The first is the digestion. Bauxite is heated together with aqueous solution of sodium hydroxide within special digesters where hydrous alumina dissolves to form sodium aluminate solution – equilibrium of reaction (1) shifts to the right. Digester temperature is set from the interval of 140–240 °C depending on bauxite composition. During the second stage known as clarification, the resulting liquor is purified from red mud (insoluble residue). The mud is then thickened and washed to recover the alkali, which is sent back to the digestion process. The third stage is precipitation, in which aluminum hydroxide at temperatures about 45–70 °C is precipitated – equilibrium of reaction (1) shifts to the left. And finally, aluminum hydroxide is calcined at temperatures about 1150–1300 °C to produce alumina during the so-called calcination stage.

Prime cost of alumina is assembled from bauxite cost, auxiliary raw (alkali, limestone and other) cost, energy (thermal and electrical) cost, investment cost, wage cost and repair bill. Approximate cost distribution for alumina is shown in Table 4 [70]. Energy intensity of alumina is estimated to range from 7 to 35 MJ/t [69–72] depending on bauxite quality and alumina refining technology.

#### 2.3. Aluminum smelting

Such standard methods of metal production as carbon reduction or electrolysis from aqueous solution are unsuitable for aluminum. Carbon reacts with aluminum producing aluminum carbide; in the process of electrolysis within aqueous solutions the hydrogen is reduced on the cathode instead of aluminum because aluminum is more electronegative.

For aluminum electrolysis the cryolite (Na<sub>3</sub>AlF<sub>6</sub>) was established to be the best electrolyte. Cryolite does not contain metals, which can be precipitated on the cathode instead of aluminum. It has a density less than that of aluminum at operating temperatures: at 950–1000 °C the density of cryolite is less than  $2.1\,\mathrm{g/cm^3}$ , while aluminum density at these temperatures is about  $2.3\,\mathrm{g/cm^3}$  [73] that positively influences on aluminum sedimentation within the electrolyzer.

Theoretically, cryolite isn't consumed during the electrolysis. However, practically, at least 20 kg of cryolite materials (Na<sub>3</sub>AlF<sub>6</sub>, AlF<sub>3</sub>, NaF) per a kg of aluminum are added into electrolysis bath [69]. Cryolite is not so abundant and for industrial purposes it is produced from fluorspar (CaF<sub>2</sub>).

Molten cryolite dissociates into ions in the following way:

$$Na_3AlF_6 \rightarrow 3Na^+ + AlF_6^{3-}$$

Alumina dissociation can be described by the following equation:

$$Al_2O_3 \to \ 2Al^{3+} + 3O^{2-}.$$

Al<sup>3+</sup> and Na<sup>+</sup> ions are moved to the cathode, but mainly aluminum ions are discharged because they are more electropositive:

$$Al^{3+} + 3e^- \rightarrow Al$$
.

 $\mbox{\rm AlF}_{6}{}^{3-}$  and  $\mbox{\rm O}^{2-}$  are moved to the anode, where oxygen ions are discharged:

$$20^{2-} - 4e^- \rightarrow 0_2$$
.

Overall process of aluminum electrolysis is described by the following equation:

$$Al_2O_3 \rightarrow 2Al + 1.5O_2.$$
 (2)

Eq. (2) corresponds to electrolysis, in which the anode is nonconsumable – inert (based on platinum, ferrite, nitride or other). However, industrial process, the Hall-Héroult process, is based on carbon anodes. Electrolyzers based on inert anode still represent the field of research and development [74–81].

Hall-Héroult process can be described by the following equation:

$$Al_2O_3 + nC \rightarrow 2Al + (3-n)CO_2 + (2n-3)CO.$$
 (3)

Industrial anodes are composed of calcined coke (70–80 wt.%) and pitch (14–35 wt.%) as a binder [73]. Two different anode types are currently used: self-baking and prebaked. Anode consumption rate ranges from 0.4 to 0.5 kg of carbon per a kg of aluminum depending on anode type and electrolysis conditions [73]. Resulting anodic gas is composed of 30–50% CO and 50–70% CO<sub>2</sub>. About 8 kg of CO<sub>2</sub>-equivalent (including emissions from power plants) per a kg of aluminum are released when aluminum is electrolytically produced [82–84].

The use of inert anodes is intended to make the aluminum production more environmentally friendly. However, smelting based on inert anode requires more electrical energy than carbon-based smelting: theoretically, the minimum energy requirement for process (2) is 51% higher than the process (3) requirement [69].

The necessary charge is defined from Faraday's law:

$$q = \frac{A}{z \times F},\tag{4}$$

where q – electrochemical equivalent, A – atomic mass, Z – valency, F – Faraday's constant. In case of aluminum Eq. (4) gives the following:

$$q = \frac{26.98154}{3 \times 96485.309} = 9.3215 \times 10^{-5} \frac{g}{A \times s}$$

i.e., theoretically, 1 Ah should produce 0.335 g of aluminum. But, practically, the mass of aluminum produced is less then theoretical value. Electrolyzers with self-baking anodes have 88% current efficiency, electrolyzers based on prebaked anodes reach 91–94% current efficiency [85]. Electrical energy intensity of aluminum varies from 13.4 kWh/kg for state-of-the-art electrolyzing technologies up to more than 20 kWh/kg for older plants [69].

# 2.4. Material and energy balance

Material balance for primary aluminum production process is schematically shown in Fig. 1. 4 kg of bauxite give about 2 kg of alumina, which then give about 1 kg of aluminum.

The energy required to raw materials preparing and aluminum smelting was estimated to be 85.6 MJ/kg of aluminum [69]. It is summed of 56 MJ of electrical energy and 29.6 MJ required for raw materials. Raw materials energy is composed of 1.1 MJ for bauxite mining, 26.1 MJ for alumina refining and 2.4 MJ for carbon anode production. Since the heat content of carbon required per a kg of

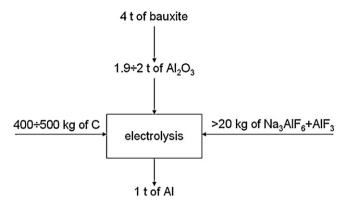


Fig. 1. Material balance for primary aluminum production.

aluminum is approximately 14 MJ, the total energy intensity of aluminum amounts to about 100 MJ/kg. The composition of aluminum energy intensity is shown in Fig. 2.

#### 2.5. Advanced aluminum production

Aluminum industry produces metal in the form of ingots unsuitable for most aluminum applications including aluminum-based energy generation technologies.

The final energy intensity of applicable aluminum depends on further processing techniques, which can vary considerably. It is evident that to minimize the energy intensity of final product, the number and energy intensity of processing steps must be minimized as well. The initial stage of aluminum processing is usually the melting, which is intended to remelt the ingots into the shape suitable for subsequent thermomechanical processing. The melting is the most energy intense processing operation of all post-smelting processes. Theoretical energy required to bring room-temperature aluminum to 960 °C molten metal is 1.4 MJ/kg; however, due to the heat losses of furnaces the actual spending on primary aluminum remelting amounts to 9 MJ of mainly thermal energy per one kg of finally produced aluminum [69].

The purity of primary aluminum produced in Hall-Héroult process, 99.7–99.9%, is not applicable in some cases as well. Aluminum refining is carried out mostly through the three-layer electrolysis technique. The electrolytically refined purity is 99.9–99.99%. Aluminum electrolytic refining, so-called Hoopes process, requires additionally about 20 kWh/kg of only electrical energy [73] that exceeds the electrical energy of Hall-Héroult process. Due to so high energy intensity the use of high purity metal in aluminum-based energy generation technologies is, evidently, very unwanted. Further purification is achieved by zone melting, which provides the purity of 99.999–99.9999%.

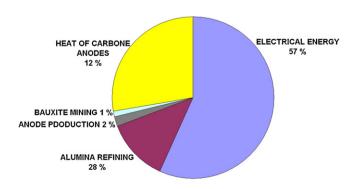


Fig. 2. Composition of aluminum energy intensity.

#### 2.6. Cycle efficiency of aluminum-based energy storage

When aluminum is oxidized to produce the energy, aluminum oxide and/or hydroxides are formed. In general, oxidation products can be returned to the aluminum smelting process. Thus, energy required for bauxite mining and alumina refining (27.2 MJ/kg in sum) can be subtracted from total energy intensity:

$$100 - 27.2 = 72.8 \,\text{MJ/kg}.$$

Calorific value of aluminum is about 31 MJ/kg. Only this energy can be usefully utilized within aluminum-fueled power plant. So, it shows the efficiency limit. If 112.8 MJ are deposited, the maximum cycle efficiency of aluminum-based energy storage is as follows:

$$\frac{31 \,\text{MJ}}{72.8 \,\text{MI}} = 43\%.$$

This percentage represents the total-thermal efficiency. Electrical energy cycle efficiency depends on the efficiency of aluminum-based energy generation technology. If only electrical energy, which is consumed in aluminum smelting (56 MJ), is taken into account and the efficiency of aluminum-based energy generation technology is assumed to be 40%, the electrical energy cycle efficiency will be:

$$\frac{31 \times 0.4 \, MJ}{56 \, MI} = 22\%.$$

It is clear, that the efficiency of aluminum-based energy storage is much smaller than that of any conventional energy technology. That is due to the combination of electrolytic and oxidation processes as in case of hydrogen. But, as compared with conventional transportable batteries, low cycle efficiency of aluminum is compensated by zero self-discharge and high energy density.

## 2.7. Perspectives of aluminum in global energy

Of course, today, in fossil fuel time, aluminum cannot be considered as the basic energy carrier instead of traditional liquid hydrocarbons. Current annual rate of primary aluminum production, about 40 million tons worldwide [56], is incomparable with global energy demands: 40 million tons of aluminum correspond to 42 million tons of coal equivalent (heat value of coal equivalent is 29 MJ/kg), while total world's energy consumption (all kinds of fuels) exceeds 10 billion tons of coal equivalent [7]. However, from bauxite resources (55–75 billion tons) it follows that the potential resource of aluminum is 14–19 billion tons or 15–20 billion tons of coal equivalent that means that, potentially, aluminum can be highly integrated into global energy.

Aluminum-based energy storage can participate as a buffer practically in any electricity generating technology. Today, aluminum electrolyzers are powered mainly by large conventional units such as coal-fired (about 40%), hydro (about 50%) and nuclear (about 5%) power plants [69,86–88]. In this field aluminum can play a role of strategic energy buffer. Due to zero self-discharge aluminum is a long term storageable and manoeuvrable fuel, which can be utilized on demand promptly. In future, if inert anodes are developed, aluminum production technology can be also integrated into distributed energy.

#### 3. Aluminum-based energy generation technologies

Aluminum has two main oxidants: oxygen and water. In accordance with Hess's law the total heat generation in aluminum—water and hydrogen—oxygen reactions equals to heat generation in aluminum—oxygen reaction.

There are many investigations in the field of aluminum combustion in atmospheric oxygen [89–100]. They are related to

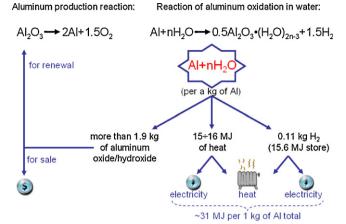


Fig. 3. Aluminum-water reaction for energy/hydrogen production.

either reaction mechanism [92–96] or reaction kinetics [97–100]. Aluminum–oxygen chemical combustion represents ungovernable high-temperature process. Therefore, the use of aluminum–oxygen combustion within non-military thermopower plant is still far from reliability. Now, this method is applied only in pyrotechnic and solid propellants [101,102].

There is another state in case of water. Due to relatively low operation temperatures, controllability and fuel cell (FC) growth, the use of water as oxidant in aluminum-based energy generation technologies attracts more attention. The energy distribution within aluminum-water reaction is shown in Fig. 3. When aluminum reacts with water, 15–16 MJ of heat, 0.111 kg of  $\rm H_2$  and over 1.9 kg of aluminum oxide/hydroxide are produced per a kg of aluminum. Precise heat and product composition depend on thermodynamic conditions (temperature and pressure) of aluminum-water reaction.

The energy stored in aluminum can be used in a wide spectrum of energy applications: from portable power sources to transport and stationary power plants. Each application is characterized by its own properties that influences on the technology. Generally, aluminum-based energy generation technologies can be categorized by aluminum oxidation method. First of all, these methods can be divided into two following categories:

- direct electrochemical (anodic) oxidation of aluminum;
- chemical aluminum-water reaction.

Let's review them.

# 3.1. Electrochemical oxidation of aluminum

The process of anodic oxidation of aluminum was opened in 1857 [103]. Since then a great number of electrochemical sources with aluminum-based anodes have been developed.

The most perspective aluminum-based battery in the view of mass usage is assumed to be aluminum-air FC battery. The oxidant in such FC is usually atmospheric oxygen. Electrolyte represents alkaline, saline or acidic aqueous solution.

The cathodic reaction of aluminum—air FC represents the oxygen reduction reaction:

$$O_2 + 2H_2O + 4e \rightarrow 4OH^-$$

Typical catalysts for this reaction are platinum, silver, metal nitrides such as  $Mn_4N$ ,  $Fe_2N$ , CrN, manganous oxide [104,105], composite oxides with spinel [106–109] or perovskite [110,111] structure, pyrolyzed macrocycles [112–114] and activated carbon [115,116]. Oxygen reduction reaction is mainly carried out on

advanced-surface electrodes, e.g. porous; active layer is generally composed of catalyst, water repelling and current conducting components.

The overall aluminum-air FC reaction can be simplified as follows:

$$4Al + 3O_2 + 6H_2O \rightarrow 4Al(OH)_3$$

In FC with saline electrolyte the anodic process of aluminum dissolution can be described by following equation:

$$Al \rightarrow Al^{3+} + 3e$$

In saline electrolyte Al<sup>3+</sup> is balanced by chloride ions, hydroxo and/or hydroxyl ions.

In FC with alkaline electrolyte the anodic process of aluminum dissolution leads to  $Al(OH)_4$  formation:

$$Al + 4OH^{-} \rightarrow Al(OH)_{4}^{-} + 3e$$
 (5)

The anodic process of aluminum dissolution is accompanied with the cathodic process of hydrogen reduction:

$$2H_2O \rightarrow H_2 + 2OH^- - 2e,$$
 (6)

This process known as corrosion reaction takes place on areas, where impurities such as copper, iron and silicon are localized [117,118]. It is accepted that corrosion reaction is parasitic process, which reduces the Coulombic efficiency of the anode, and must be necessarily suppressed. To minimize the corrosion reaction the anode is proposed to be produced from high-purity aluminum (with the purity not less than 99.995%) or the certain impurities must be reduced, e.g. iron [119]. However, the cost of such aluminum was estimated to be almost two times more than the cost of 99.9% purity aluminum [120]. So, it is clear, that anode based energy generation technology faces directly with the problem relating to high purity aluminum. To increase the cycle efficiency of aluminum-based energy storage, high purity aluminum must be replaced by aluminum of technical purity.

The efficiency of aluminum-air FC is increased when aluminum is alloyed with special elements such as Ga, In, Sn, Zn, Pb, Mg, Mn. It was established that such elements move the anode potential to negative field, decrease the polarization (at fixed potential current) or increase the current density (at fixed potential) of aluminum-air FC [121-138]. The improvement of anode performance by additional elements is known as activation. Activation leads to the oxide film thickness and/or composition changing or to oxide film destruction. It is achieved not only by certain composition but also by alloy preparation quality. So in [136] it was shown that alloys, which have the similar composition, can differ in electrochemical characteristics that was explained by different preparation techniques. There was also claimed that 99.98% aluminum alloy with Mg (0.6 wt.%), Sn (0.1 wt.%) and Ga (0.05 wt.%) in 2 M NaCl solution can be stable against the corrosion at room temperature for several weeks.

Activation of the anode is also achieved with the help of electrolyte additions. The influence of such additions as CaO and CaCl<sub>2</sub>, sodium citrate (Na<sub>3</sub>C<sub>6</sub>H<sub>5</sub>O<sub>7</sub>) and stannate (Na<sub>2</sub>SnO<sub>3</sub>) on anode performance in 4 M alkaline solution was studied in [119,132,139,140]. All of these additions was claimed to improve the behavior of anode and allow using technical purity aluminum at optimized electrolyte composition. Technical purity aluminum was also used in [121,141], where the speed of corrosion was studied in alkaline electrolyte containing ZnO. 98.7% aluminum alloy with Mn (1.2 wt.%) and 97.5% aluminum alloy with Mg (2 wt.%) and Mn (0.25 wt.%) were found to be the suitable anode materials; 6 M ZnO was found to be the best concentration in 4 M NaOH solution. The deposition of zinc on the anode was found to strengthen in composite electrolyte with organic additions [142,143]. In [143–146]

it was proposed to use methanol as corrosion inhibitor. The speed of corrosion reaction in saline and acid electrolytes was shown to decrease also when certain ions such as Hg<sup>2+</sup>, Ga<sup>3+</sup>, In<sup>3+</sup>, Sn<sup>2+</sup>, Zn<sup>2+</sup> were added into electrolyte [135,147–152].

In [42,117,153,154] the hydrogen produced during corrosion was proposed to be utilized in air–hydrogen FC. That was aimed to increase the overall electrical efficiency of a combined system and in the long run to use low grade aluminum in anode manufacturing.

Besides aluminum-air FC the aluminum as anode is used in such systems as Al-H<sub>2</sub>O<sub>2</sub>, Al-MnO<sub>2</sub>, Al-AgO and Al-S. These systems apply aqueous solutions as well. Another type of electrolyte for aluminum-based anodes is molten salt. The use of molten salt is intended mainly for rechargeable technologies. Operation principle and technical characteristics of these types batteries were considered in [155].

Although theoretical energy density of generation technology based on aluminum-air FC battery is about 4300 Wh/kg and electrical efficiency is about 55% [154], the actual specific energy and efficiency are 300 Wh/kg and 45% [117,154,156] respectively.

Today, mainly lead-acid [10,11], nickel-metal hydride [14] and lithium-ion [18] batteries are planned to remove the internal combustion engines in transport sector. But, low specific characteristics, high self-discharge rate, short lifetime and high cost prevent them from scale integration into transport. The specific energy of aluminum-air FC battery has been already higher than that of transport-intended conventional accumulators, while the recharge of aluminum-air FC battery vehicle is easy as well. So, if other vital questions such as self-discharge and material cost are decided in case of aluminum-air FC battery, it can potentially compete with both internal combustion engine and other electrochemical accumulators.

#### 3.2. Aluminum-water reaction

# 3.2.1. Aluminum-water reaction in alkaline solution

Hydrogen production method based on aluminum oxidation in alkaline aqueous solutions is one of the oldest and more than century-known as well [157–159]. The process of hydrogen generation in this case goes through electrochemical reactions (5) and (6). Overall reaction is described by following equation:

$$2AI + 6H_2O \rightarrow 2AI(OH)_3 + 3H_2$$
 (7)

The kinetics of aluminum oxidation in alkaline aqueous solutions is a topic of many investigations, which have been continuing up to now [160–167]. Due to NaOH, KOH, Ca(OH)<sub>2</sub> comparison [165] it was established that NaOH is the best hydroxide for aluminum alloys oxidation in the view of reaction rate and conversion degree. To reach the same reaction rates in case of KOH the higher alkali concentration or temperature as compared with NaOH are required [164]. Kinetics of aluminum oxidation in NaOH solution depending on molar ratio NaOH/Al was studied in [160,162,167]. From those works it can be concluded that optimal conditions for this reaction are 70-90 °C and 5.75 M NaOH solution. Hydrogen yield and reaction rate increase when sodium aluminate (NaAlO<sub>2</sub>) solution instead of NaOH is used at the same pH level [163]. In [168] aluminum oxidation in NaAlO2 solution with Al(OH)3 additions was studied. It was established that Al(OH)<sub>3</sub> prevents the oxide film growing on the surface of aluminum particles that in the long run accelerates the chemical reaction.  $0.01 \,\mathrm{M} \,\mathrm{NaAlO}_2 + 20 \,\mathrm{g/dm}^3$  $Al(OH)_3$  were chosen as optimum (pH = 12); maximum hydrogen generation rate was 200 cm<sup>3</sup>/min per a gram of aluminum. Oxidation kinetics of different aluminum-based alloys in alkaline aqueous solutions was studied in [165,169]; it was determined that Al-Si alloys have the most oxidation rate and conversion degree. In [166] it is claimed that the mixture of aluminum (its alloys) and sodium borohydride (NaBH<sub>4</sub>) is the perspective matter for

hydrogen generation, because the hydrolysis of NaBH<sub>4</sub> increases the pH of aqueous solution while aluminum alloys have a catalytic influence on the hydrolysis process.

The reaction of aluminum oxidation in alkaline solutions has been already applied in a great number of hydrogen generators [157,158,160,161,170–178] and energotechnological plants [161,179,180].

The design of co-generation energotechnological plant based on aluminum oxidation in alkaline solution, was described in [161]. In [177] it was shown that the hydrogen produced during aluminum waste cans oxidation in 2 M NaOH aqueous solution can be successfully utilized in air-hydrogen FC. FC in that case showed better electrical characteristics than in case when it was fed by hydrogen from proton exchangeable membrane electrolyzer. Hydrogen generators combined with air-hydrogen micro-FC was shown to suit for portable power sources [178].

The efficient recycling of waste aluminum was proposed in [161,180]. Aluminum is utilized within the special reactors filled with NaOH solution at high pressures (up to 30 MPa) and relatively moderate temperatures (to 150 °C) to produce high-purity compressed hydrogen and marketable aluminum hydroxide. Aluminum hydroxide is supposed to return to aluminum metallurgy or go into market of inorganic materials (Fig. 3). Possible design and operation principle of such reactors are shown in [181]. High thermodynamic (up to 90%) and economic efficiencies of such co-generation approach proved in exergetic life cycle assessment [179].

Aluminum-fueled adsorption refrigeration plant was proposed in [182]. In that plant the scrap aluminum as fuel and alkaline aqueous solution as oxidant were used for hydrogen production. Hydrogen was then chemically combusted to produce the heat, which is then utilized within ammonia–water cycle: increase the speed of separation of ammonia from water.

Main advantages of aluminum oxidation in alkaline solution are simplicity and relatively low cost of necessary reagents and equipment. The technologies, which are based on this oxidation method, can be applied in portable field, transport and stationary. But, probably the single and at the same time the essential disadvantage of this method is high corrosiveness of working medium.

#### 3.2.2. Mechanochemical activation of aluminum

This type of aluminum activation supposes to use additional chemical substances whose physicochemical properties influence on aluminum reactivity.

One of the oldest methods of chemical activation of aluminum is amalgamation [183,184]. 3–5 wt.% hydrargyrum addition increases the hydrogen production rate up to  $1440\,\mathrm{cm^3/min}$  per a gram of aluminum [185]. However, the toxicity of this approach prevents it from practice.

The activity of aluminum in water increases by alloying with different metals such as Ga, In, Re, Bi, Mg, Ca [186–192]. The additions act specifically on mechanical strength of cast solid due to adsorptive penetration, so-called Rebinder effect [193]. Such activation allows carrying out the aluminum–water reaction at relatively moderate temperatures. Multi-element aluminum-based alloys doped with Zn, Sn, Ga and In were studied in [190,191]. Although the alloys showed an appropriate oxidability with 96% conversion degree after 0.5 h, the cast solid suffered from the necessity of its cryogenic storage (at liquid nitrogen temperatures) [190]. This problem is solved by mechanochemical activation of aluminum [186,192]. After this activation the reagent can be stored under room temperatures. The reaction time of mechanochemically activated aluminum is several minutes, while the conversion degree nears to theoretical value.

Another mechanochemical activation of aluminum is NaCl doping [194–197]. The study of microstructure, specific surface area

and chemistry of aluminum powder doped with NaCl is presented in [194]. In [196] it was established that optimal NaCl to Al mass ratio is 2; average speed of hydrogen generation increases from 100 to  $200\,\mathrm{cm^3/min}$  per a gram of aluminum with temperature increasing from  $55\,^\circ\mathrm{C}$  to  $70\,^\circ\mathrm{C}$ .

Mechanochemical activation of aluminum was proposed to be used in special cartridges to produce hydrogen for portable air–hydrogen FC [197–200]. Some prototypes of aluminum-based portable power sources with air–hydrogen FC have been already made [198–200].

#### 3.2.3. Mechanical activation of aluminum

Aluminum can react with water and produce hydrogen also due to mechanical activation [98,201,202]. It implies no chemical additions and can be divided into in-process activation and pre-activation.

The concept of in-process activation is described in [201,202]. Activation process and aluminum oxidation occurs simultaneously. Activation may represent cutting, grinding or other. It implies that fresh uncovered by oxide film surface of aluminum, which is produced during activation, immediately falls into oxidative medium. During in-process activation the aluminum is oxidized due to pitting corrosion. The use of wet cutting of aluminum alloys was proposed for hydrogen generation in [201].

By preliminary mechanical activation here, the production of ultra dispersed aluminum powder is implied. This activation represents the stand-alone processing characterized by high energy consumption. Ultrafine aluminum powder is produced today generally by electrical explosion of aluminum wire [203–206], plasma-based atomization [207–209], inductive method [210], aluminum reduction from its halides in alkali steam [211–213] and decomposition of metalorganic compounds [214–216].

Industrially produced aluminum powders are shown to be unsuitable for aluminum–water reaction at relatively moderate temperatures [217,218]. The conversion degree of aluminum micron powder in pure, without any activation additions, water at temperatures below  $100\,^{\circ}\text{C}$  is far from 100%. After 5 h staying within special  $100\,^{\circ}\text{C}$  water-filled reactor under intensive mixing the conversion of aluminum powder with average particle size of  $20\,\mu\text{m}$  was less than 60% [217].

On the contrary, nano-sized aluminum powder reacts with pure, without any activation additions, water with high reaction rate and conversion degree [99,100]. The conversion of aluminum powder with average particle size of  $140 \, \mathrm{nm}$  in water at  $50-70 \, ^{\circ}\mathrm{C}$  was close to 1; the reaction time decreased from  $40 \, \mathrm{min}$  for  $50 \, ^{\circ}\mathrm{C}$  to  $20 \, \mathrm{min}$  for  $70 \, ^{\circ}\mathrm{C}$  [99].

Due to its high chemical activity, the ultrafine aluminum powder has been already proved to be an appropriate material for pyrotechnic compositions and solid propellants [101,102]. But, its use for electrical, thermal or kinetic energy production is connected with a number of drawbacks caused by the same high activity of nanoscale powders. Following the explosion characteristics comparison between aluminum micron and submicron powders it was established that the last one has bigger maximum explosion pressure, bigger maximum rate of pressure rise and smaller minimum ignition energy [219]. Ultrafine powder must be kept under inert atmosphere or special passivating films should be created on particles surface when powder is produced [220–222]. Moreover, when aluminum powder dispersity increases, the percentage of active metal and the apparent density of powder decrease [98].

Chemical and (or) mechanical activation of aluminum results in considerable rise in reagent cost. The cost of activated aluminum is increased by both the use of expensive rare metals and high power consumption. Therefore, it is evident that the preliminary activated aluminum cannot compete with oil and the field of its application is only portable. From available 31 MJ/kg

of stored in aluminum energy, maximum half can be really converted into electrical energy, because the effective utilization of heat of aluminum-water reaction in portable scale is practically impossible. Useable heat represents the chemical energy of produced hydrogen (Fig. 3) and it is converted into electrical energy with the efficiency of FC. If FC efficiency is 50%, a kg of aluminum returns about 7.5 MJ of electrical energy (about 25% from available energy stored in aluminum). So, if the stoichiometric water is taken into account, the theoretical energy density of the system based on activated aluminum is about 2.5 MJ/kg (700 Wh/kg). If water, which is produced in air–hydrogen FC, is supposed to return from FC to aluminum–water reaction, the energy density will be increased to 3.75 MJ/kg (1040 Wh/kg) that considerably exceeds energy densities of conventional batteries.

#### 3.2.4. High-temperature aluminum-water reaction

Aluminum—water reaction can be initiated by high temperatures. Due to high temperatures the aluminum can be used in the form of micron powders, which are produced from the melt by standard pulverization method [223]. So, the production of micron powder needs less energy than ultrafine powder production.

Mechanism and kinetics of high-temperature aluminum—water reaction were studied recently within the combustion theory [92–100,224–227]. It was established that aluminum combustion in water differs considerably from combustion in air. In [100] spherical aluminum particles with average size of 3–4.5  $\mu m$  when linearly heated (at rates of 1–20 °C/min) in waterlogged air were totally oxidized before 1000 °C while in dry oxygen the reaction finished at 1500 °C.

Aluminum–water reaction at stoichiometric mass ratio goes, theoretically, under about 3000 °C. High-temperature hydrogen produced was proposed to be used in magnetohydrodynamic generator [228,229]. However, although this method promises high thermodynamic efficiency (about 40%), for date it has been only theoretically evaluated and doesn't have practical realization.

Kinetics of aluminum oxidation in wet steam of water at temperatures before  $250\,^{\circ}\text{C}$  was studied in [230]. Reaction time and conversion degree of aluminum powder with average particle size of  $24\,\mu\text{m}$  were explored depending on steam temperature. Maximum conversion degree was found to be 80%, while the reaction lasted several hours.

Oxidation kinetics of aluminum micron powder in boiling water at temperatures 230–370 °C was studied depending on powder size and temperature in [231]. It was established that aluminum powder with average particle size up to 70  $\mu m$  is intensively oxidized in boiling water at temperature over 230 °C, the conversion degree is close to 100% and the reaction lasts only several tens of seconds. That method laid the basis for the technology of hydrogen, heat and aluminum oxide/hydroxide co-production [232–234]. An experimental power plant created had 12% electrical efficiency and about 70% total efficiency [235].

Thermodynamic efficiency of aluminum-water reactors as steam-hydrogen generators was studied in [181,236–239]. Theoretical investigations showed both high electrical efficiency (up to 40–45%) and high total efficiency (60–80%).

Aluminum micron powder oxidation in seawater was proposed for the creation of submarine propulsion system [240]. It is based on aluminum–water reactor and steam–hydrogen turbine. Steam–hydrogen mixture produced within the reactor speeds up the turbine. Temperature and pressure of steam–hydrogen mixture before turbine are 800–1000 °C and 2–5 MPa respectively. Although the propulsion system is just theoretically developed, some of its components have been already tested.

Co-generation power plant based on high-temperatures aluminum oxidation in water steam was modeled in [241]. High-pressure steam-hydrogen mixture goes from the reactor into

**Table 5**Summary of aluminum-based energy generation technologies.

Oxidation method	Application areas	Electrical efficiency (related to aluminum calorific value), %	Energy density, Wh/kg	Priority problems
Electrochemical oxidation of aluminum	Portable, Transport, Stationary	55	4300	High purity aluminum
Aluminum-water reaction in alkaline solution	Portable, Transport	25	1040	Designing
	Stationary	45	8600	
Mechanochemical activation of aluminum	Portable	25	1040	Use of rare metals, High energy intensity
Mechanical activation of aluminum	Portable	25	1040	High energy intensity
High-temperature aluminum-water reaction	Stationary	45	8600	Designing

the turbine and then from the turbine into the heat exchanger. Power plant is evaluated to produce 80 kW of electrical and 130 kW of thermal energy. Theoretical power plant total efficiency is 40%.

Due to relatively high temperatures, main applicable fields for this technology are stationary and probably transport. If water is supposed to be present on site where energy is produced, the energy density of aluminum-based energy storage will be equal to that of aluminum (8600 Wh/kg), because in this case only the metal needs to be stored and transported. High temperature of reaction products, in particular steam—hydrogen mixture, provides high thermodynamic efficiency of aluminum—based energy generation. The use of industrial powders is an efficient aluminum—based energy storage technology, because energy intensity of these powders is most close to energy intensity of primary aluminum.

#### 3.3. Oxidation methods summary

The summary of aluminum-based energy generation technologies is presented in Table 5.

# 4. Conclusion

Main conclusions, which can be marked from this work, are as follows:

- Global energy is ever-changing organism. Today, as never before, this organism needs to store the at all scales: from portable and transport to large stationary. Energy storage technologies are required to remove the oil from transport, to support the renewable, distributed and Smart-grid energy and to smooth the load of conventional power plants.
- 2. Although there are a great number of commercially available energy storage technologies, none of them can be referred to as universal and each has its own specialized application areas. Moreover, there are no appropriate transportable energy storage technologies, which might compete with oil in its traditional niches (transport and small stationary).
- 3. Hydrogen is proposed to be used as energy storage and carrier. But, storage and transportation of hydrogen are still open problems, as several decades ago.
- 4. In this work aluminum was considered as energy storage and carrier. To produce 1 kg of aluminum, 2 kg of alumina, 0.4–0.5 kg of coal, 0.02–0.08 kg of cryolite and 13.4–20 kWh of electrical energy are required. Total energy intensity of aluminum was estimated to be about 100 MJ/kg. Cycle efficiency of aluminum-based energy storage does not exceed 43%.
- 5. Although aluminum production is very energy intensive process with high greenhouse gas emissions, some physical-chemical properties of aluminum are very attractive for energy storage and carrying. Among them there are zero self-discharge and high

- energy density. Aluminum can be stored for a long time and transported to any distance.
- There are a number of aluminum-based energy generation technologies. Different technologies are based on different aluminum oxidation methods and intended for different application areas.
- 7. For portable applications the most appropriate solutions are electrochemical oxidation of aluminum, aluminum—water reaction in alkaline solution and oxidation of activated (mechanochemically or mechanically) aluminum. Direct electrochemical oxidation has, theoretically, 4300 Wh/kg energy density and about 55% electrical efficiency. Technologies based on chemical aluminum oxidation can reach 1040 Wh/kg energy density and 25% electrical efficiency. Electrochemical oxidation of aluminum and aluminum—water reaction in alkaline solution suit also for transport.
- 8. Stationary is for high-temperature aluminum—water reaction and aluminum—water reaction in alkaline solution. Theoretical electrical efficiency is about 45%, while energy density equals to its maximum value, 8600 Wh/kg, because transportation to stationary power plant is assumed to be required only for aluminum.
- 9. Today, aluminum cannot be considered as the basic energy carrier instead of traditional liquid hydrocarbons. It might be highly integrated into global energy in post-fossil fuel era. But, there are a number of special aluminum-based applications already for today. The coming of aluminum-based energy storage technologies is expected in some portable applications and small-power eco-cars. Since energy generation based on aluminum is cleaner than that of fossil fuel, the use of aluminum is defensible within polluted areas, e.g. within megapolises. Aluminum can be applied also in remote non-electrified areas, disaster areas, within ground and underground systems of defense infrastructure and within power systems of ships including submarines. Another today's perspective application is hydrogen and aluminum oxide/hydroxide co-production technology.

# References

- [1] Campbell CJ, Laherrère JH. The end of cheap oil. Scientific American 1998:278:78–83.
- [2] Aleklett K, Höök M, Jakobsson K, Lardelli M, Snowden S, Söderbergh B. The peak of the oil age – analyzing the world oil production reference scenario in World Energy Outlook 2008. Energy Policy 2010;38:1398–414.
- [3] de Almeida P, Silva PD. The peak of oil production—timings and market recognition. Energy Policy 2009;37:1267–76.
- [4] Verbruggen A, Al Marchohi M. Views on peak oil and its relation to climate change policy. Energy Policy 2010;38:5572–81.
- [5] Bridge G. Geographies of peak oil: the other carbon problem. Geoforum 2010;41:523–30.
- [6] Hirsch RL. Mitigation of maximum world oil production: shortage scenarios. Energy Policy 2008;36:881–9.
- [7] World Energy Outlook 2010: International Energy Agency; 2010.
- [8] Parker CD. Lead-acid battery energy-storage systems for electricity supply networks. Journal of Power Sources 2001;100:18–28.

- [9] Martha S, Hariprakash B, Gaffoor S, Trivedi D, Shukla A. A low-cost lead-acid battery with high specific-energy. Journal of Chemical Sciences 2006:118:93–8.
- [10] Conte M, Pede G, Sglavo V, Macerata D. Assessment of high power HEV leadacid battery advancements by comparative benchmarking with a European test procedure. Journal of Power Sources 2003;116:118–27.
- [11] Cooper A. Development of a lead-acid battery for a hybrid electric vehicle. Journal of Power Sources 2004;133:116–25.
- [12] Wen Z, Cao J, Gu Z, Xu X, Zhang F, Lin Z. Research on sodium sulfur battery for energy storage. Solid State Ionics 2008;179:1697–701.
- [13] Shukla AK, Venugopalan S, Hariprakash B. Nickel-based rechargeable batteries. Journal of Power Sources 2001;100:125–48.
- [14] Taniguchi A, Fujioka N, Ikoma M, Ohta A. Development of nickel/metalhydride batteries for EVs and HEVs. Journal of Power Sources 2001;100:117-24.
- [15] Ritchie A, Howard W. Recent developments and likely advances in lithium-ion batteries. Journal of Power Sources 2006;162:809–12.
- [16] Zackrisson M, Avellán L, Orlenius J. Life cycle assessment of lithium-ion batteries for plug-in hybrid electric vehicles – critical issues. Journal of Cleaner Production 2010;18:1519–29.
- [17] Nazri G-A, Pistoia G. Lithium batteries: science and technology. New York: Springer Science+Business Media; 2003.
- [18] Tamura K, Horiba T. Large-scale development of lithium batteries for electric vehicles and electric power storage applications. Journal of Power Sources 1999;81–82:156–61.
- [19] Joerissen L, Garche J, Fabjan C, Tomazic G. Possible use of vanadium redoxflow batteries for energy storage in small grids and stand-alone photovoltaic systems. Journal of Power Sources 2004;127:98–104.
- [20] Rydh CJ. Environmental assessment of vanadium redox and lead-acid batteries for stationary energy storage. Journal of Power Sources 1999;80:21–9.
- [21] Mohamed MR, Sharkh SM, Walsh FC. Redox flow batteries for hybrid electric vehicles: progress and challenges. In: Vehicle Power and Propulsion Conference, 2009 VPPC '09 IEEE. 2009. p. 551–7.
- [22] Shukla AK, Sampath S, Vijayamohanan K. Electrochemical supercapacitors: energy storage beyond batteries. Current Science 2000;79:1656–61.
- [23] Hassenzahl W. Will superconducting magnetic energy storage be used on electric utility systems? IEEE Transactions on Magnetics 1975;11:
- [24] Bolund B, Bernhoff H, Leijon M. Flywheel energy and power storage systems. Renewable and Sustainable Energy Reviews 2007;11:235–58.
- [25] Liu H, Jiang J. Flywheel energy storage—an upswing technology for energy sustainability. Energy and Buildings 2007;39:599–604.
- [26] Deane JP, Ó Gallachóir BP, McKeogh EJ. Techno-economic review of existing and new pumped hydro energy storage plant. Renewable and Sustainable Energy Reviews 2010;14:1293–302.
- [27] Kim YM, Favrat D. Energy and exergy analysis of a micro-compressed air energy storage and air cycle heating and cooling system. Energy 2010;35:213–20.
- [28] Lund H, Salgi G. The role of compressed air energy storage (CAES) in future sustainable energy systems. Energy Conversion and Management 2009:50:1172-9.
- [29] Saidur R, Rahim NA, Hasanuzzaman M. A review on compressed-air energy use and energy savings. Renewable and Sustainable Energy Reviews 2010;14:1135-53
- [30] Chen H, Cong TN, Yang W, Tan C, Li Y, Ding Y. Progress in electrical energy storage system: a critical review. Progress in Natural Science 2009:19:291–312.
- [31] Hadjipaschalis I, Poullikkas A, Efthimiou V. Overview of current and future energy storage technologies for electric power applications. Renewable and Sustainable Energy Reviews 2009;13:1513–22.
- [32] Ibrahim H, Ilinca A, Perron J. Energy storage systems—characteristics and comparisons. Renewable and Sustainable Energy Reviews 2008;12:1221–50.
- [33] Beaudin M, Zareipour H, Schellenberglabe A, Rosehart W. Energy storage for mitigating the variability of renewable electricity sources: an updated review. Energy for Sustainable Development 2010;14:302–14.
- [34] Baker J. New technology and possible advances in energy storage. Energy Policy 2008;36:4368–73.
- [35] Smith SC, Sen PK, Kroposki B. Advancement of energy storage devices and applications in electrical power system. Power and Energy Society General Meeting – Conversion and Delivery of Electrical Energy in the 21st Century, 2008 IEEE2008, p. 1–8.
- [36] Hall PJ, Bain EJ. Energy-storage technologies and electricity generation. Energy Policy 2008;36:4352–5.
- [37] Huang K-L, Li X-g., Liu S-q., Tan N, Chen L-q. Research progress of vanadium redox flow battery for energy storage in China. Renewable Energy 2008;33:186–92.
- [38] Will FG. Impact of lithium abundance and cost on electric vehicle battery applications. Journal of Power Sources 1996;63:23–6.
- [39] Nejat Veziroglu T, Sherif SA, Barbir F. Hydrogen energy solutions. In: Franklin JA, Nelson Leonard N, editors. Environmental solutions. Burlington: Academic Press; 2005. p. 143–80.
- [40] Nejat V, lu T. Hydrogen technology for energy needs of human settlements. International Journal of Hydrogen Energy 1987;12:99–129.
- [41] Auner N, Holl S. Silicon as energy carrier—facts and perspectives. Energy 2006;31:1395–402.
- [42] Sheindlin A, Zhuk A. Concept of aluminum hydrogen energy industry. Russian Journal of General Chemistry 2007;77:778–82.

- [43] Mignard D, Pritchard C. A review of the sponge iron process for the storage and transmission of remotely generated marine energy. International Journal of Hydrogen Energy 2007;32:5039–49.
- [44] Yabe T, Uchida S, Ikuta K, Yoshida K, Baasandash C, Mohamed MS, et al. Demonstrated fossil-fuel-free energy cycle using magnesium and laser. Applied Physics Letters 2006;89:261107–13.
- [45] Cowey K, Green KJ, Mepsted GO, Reeve R. Portable and military fuel cells. Current Opinion in Solid State and Materials Science 2004;8:367–71.
- [46] Ross DK. Hydrogen storage: the major technological barrier to the development of hydrogen fuel cell cars. Vacuum 2006;80:1084–9.
- [47] Schulten R. Nuclear energy as a primary energy source for hydrogen production. International Journal of Hydrogen Energy 1980;5:281–92.
- [48] Elder R, Allen R. Nuclear heat for hydrogen production: coupling a very high/high temperature reactor to a hydrogen production plant. Progress in Nuclear Energy 2009;51:500–25.
- [49] Fujiwara S, Kasai S, Yamauchi H, Yamada K, Makino S, Matsunaga K, et al. Hydrogen production by high temperature electrolysis with nuclear reactor. Progress in Nuclear Energy 2008;50:422–6.
- [50] Utgikar V, Thiesen T. Life cycle assessment of high temperature electrolysis for hydrogen production via nuclear energy. International Journal of Hydrogen Energy 2006;31:939–44.
- [51] Vanderryn J, Salzano FJ, Bowman MG. International cooperation on development of hydrogen technologies. International Journal of Hydrogen Energy 1977:1:357–63.
- 1977;1:357-65.
  [52] Zhou L. Progress and problems in hydrogen storage methods. Renewable and Sustainable Energy Reviews 2005;9:395-408.
- [53] Bardsley W. The sustainable global energy economy: hydrogen or silicon? Natural Resources Research 2008;17:197–204.
- [54] Vargel C, Jacques M, Schmidt DMP. The corrosion of aluminium. Amsterdam: Elsevier; 2004. p. 81–109.
- [55] Dyar M, Gunter ME. Mineralogy And Optical Mineralogy Mineralogical Society of America; 2007.
- [56] Mineral commodity summaries 2010: U.S. Geological Survey; 2010.
- [57] Djukanovic G. Aluminum: world market prospects for troubled times. JOM Journal of the Minerals, Metals and Materials Society 2009;61:63–6.
- [58] Hale W. The global light metals sector outlook: a primary aluminum perspective. JOM Journal of the Minerals, Metals and Materials Society 2000;52:26–30.
- [59] Alcoa 2009 Annual Report and Form 10-K. Pittsburgh; 2009.
- [60] Goldschmidt VM. The principles of distribution of chemical elements in minerals and rocks. The seventh Hugo Muller Lecture, delivered before the Chemical Society on March 17th, 1937. Journal of the Chemical Society (Resumed) 1937:655–73.
- [61] Suess HE, Urey HC. Abundances of the elements. Reviews of Modern Physics 1956:28:53.
- [62] Liu W, Yang J, Xiao B. Review on treatment and utilization of bauxite residues in China. International Journal of Mineral Processing 2009;93:220–31.
- [63] Meyer FM, Happel U, Hausberg J, Wiechowski A. The geometry and anatomy of the Los Pijiguaos bauxite deposit, Venezuela. Ore Geology Reviews 2002;20:27–54.
- [64] Balasubramaniam KS, Surendra M, Kumar TVR. Genesis of certain bauxite profiles from India. Chemical Geology 1987;60:227–35.
- [65] Anand RR, Gilkes RJ, Roach GID. Geochemical and mineralogical characteristics of bauxites, Darling Range, Western Australia. Applied Geochemistry 1991;6:233–48.
- [66] http://www.mineral.ru/Facts/stat/124/201/index.html.
- [67] Fourth sustainable bauxite mining report: International Aluminium Institute;
- [68] Kogel JE, Trivedi NC, Barker JM, Krukowski ST. Industrial minerals & rocks. seventh ed. Society for Mining, Metallurgy, and Exploration; 2006.
- [69] Green JAS. Aluminum recycling and processing for energy conservation and sustainability. ASM International; 2007.
- [70] Ahmedov SN, Kiselev AI, Medvedev VV, Gromov BS, Pak RV, Borisoglebsky YuV. State and tendencies of development of world alumina production. Nonferrous Metals 2002:42–5 [in Russian].
- [71] Liu L, Aye L, Lu Z, Zhang P. Analysis of the overall energy intensity of alumina refinery process using unit process energy intensity and product ratio method. Energy 2006;31:1167–76.
- [72] Liu L, Aye L, Lu Z, Zhang P. Effect of material flows on energy intensity in process industries. Energy 2006;31:1870–82.
- [73] Totten GE, MacKenzie DS. Handbook of aluminum. New York: Marcel Dekker, Inc.; 2003.
- [74] Sadoway D. Inert anodes for the Hall-Héroult cell: the ultimate materials challenge. JOM Journal of the Minerals, Metals and Materials Society 2001;53:34–5.
- [75] Thonstad J, Olsen E. Cell operation and metal purity challenges for the use of inert anodes. JOM Journal of the Minerals, Metals and Materials Society 2001;53:36–8.
- [76] Mroz T. Evaluating a new material for Hall-Héroult cell cathodes. JOM Journal of the Minerals, Metals and Materials Society 1997;49:24–5.
- [77] Edwards L, Richards N, Kvande H. Inert anodes and other new Al technologies—benefits, challenges, and impact on present technology. JOM Journal of the Minerals, Metals and Materials Society 2001;53:48–50.
- [78] Edwards L, Kvande H. Inert anodes and other technology changes in the aluminum industry—the benefits, challenges, and impact on present technology. JOM Journal of the Minerals, Metals and Materials Society 2001;53:28.

- [79] Kvande H, Haupin W. Inert anodes for Al smelters: energy balances and environmental impact. JOM Journal of the Minerals, Metals and Materials Society 2001:53:29–33.
- [80] Haarberg GM, Kvalheim E, Ratvik AP, Xiao SJ, Mokkelbost T. Depolarised gas anodes for aluminium electrowinning. Transactions of Nonferrous Metals Society of China 2010;20:2152–4.
- [81] Keniry J. The economics of inert anodes and wettable cathodes for aluminum reduction cells. JOM Journal of the Minerals, Metals and Materials Society 2001;53:43–7.
- [82] Halmann M, Frei A, Steinfeld A. Carbothermal reduction of alumina: thermochemical equilibrium calculations and experimental investigation. Energy 2007;32:2420-7.
- [83] Hayashi D, Krey M. CO<sub>2</sub> emission reduction potential of large-scale energy efficiency measures in heavy industry in China, India, Brazil, Indonesia and South Africa. Hamburg: Hamburg Institute of International Economics; 2005
- [84] Choate W, Green J. Technoeconomic assessment of the carbothermic reduction process for aluminum production. Light Metals 2006;2:445–50.
- [85] Yanjia W, Chandler W. The Chinese nonferrous metals industry—energy use and CO<sub>2</sub> emissions. Energy Policy 2010;38:6475–84.
- [86] Skea J. Electricity supplies for the primary aluminium industry. Resources Policy 1980;6:60–70.
- [87] Xiao-wu W, Li-rong G, Hua B. Resources conservation—the alternative scenarios for Chinese aluminum industry. Resources, Conservation and Recycling 2008;52:1216–20.
- [88] Schwarz H-G, Briem S, Zapp P. Future carbon dioxide emissions in the global material flow of primary aluminium. Energy 2001;26:775–95.
- [89] Arkhipov VA, Ermakov VA, Razdobreev AA. Dispersity of condensed products of combustion of an aluminum drop. Combustion, Explosion, and Shock Waves 1982;18:139–42.
- [90] Fedorov BN, Plechov YL, Timokhin ÉM. Particle size of aluminum oxide particles in the combustion products of condensed substances. Combustion, Explosion, and Shock Waves 1982;18:16–9.
- [91] Gremyachkin VM. Theory of ignition of metallic particles. Combustion, Explosion, and Shock Waves 1983; 19:259–63.
- [92] Bartlett RW, Ong Jr JN, Fassell Jr WM, Papp CA. Estimating aluminium particle combustion kinetics. Combustion and Flame 1963;7:227–34.
- [93] Belyaev AF, Frolov YV, Korotkov AI. Combustion and ignition of particles of finely dispersed aluminum. Combustion, Explosion & Shock Waves 1968:4:323-9.
- [94] Breiter AL, Mal'tsev VM, Popov EI. Models of metal ignition. Combustion, Explosion & Shock Waves 1977;13:475–84.
- [95] Brustowski TA, Glassman I. Spectroscopic investigation of metal combustion. Heterogeneous combustion, New York: Academic Press: 1964 p. 41–74
- [96] Kovalev O. Adiabatic method in the thermal theory of ignition of metal particles in gases. Combustion, Explosion, and Shock Waves 1994;30: 597-600.
- [97] Bezprozvannykh V, Ermakov V, Razdobreev A. Induction period for the heating of metal particles by continuous laser radiation. Combustion, Explosion, and Shock Waves 1992;28:627–30.
- [98] Il'in AP, Gromov AA, Yablunovskii GV. Reactivity of aluminum powders. Combustion, Explosion, and Shock Waves 2001;37:418–22.
- [99] Ivanov VG, Safronov MN, Gavrilyuk OV. Macrokinetics of oxidation of ultradisperse aluminum by water in the liquid phase. Combustion, Explosion, and Shock Waves 2001:37:173–7.
- [100] Schoenitz M, Chen C-M, Dreizin EL. Oxidation of aluminum particles in the presence of water. The Journal of Physical Chemistry B 2009;113:5136–40.
- [101] Meda L, Marra G, Galfetti L, Severini F, De Luca L. Nano-aluminum as energetic material for rocket propellants. Materials Science and Engineering C 2007:27:1393–6.
- [102] Pourmortazavi SM, Hajimirsadeghi SS, Kohsari I, Fathollahi M, Hosseini SG. Thermal decomposition of pyrotechnic mixtures containing either aluminum or magnesium powder as fuel. Fuel 2008;87:244–51.
- [103] Buff H. Ueber das electrische Verhalten des Aluminiums. Justus Liebigs Annalen der Chemie 1857;102:265–84.
- [104] Fang Z-q, Hu M, Liu W-x, Chen Y-r, Li Z-y, Liu G-y. Preparation and electrochemical property of three-phase gas-diffusion oxygen electrodes for metal air battery. Electrochimica Acta 2006;51:5654–9.
- [105] Calegaro ML, Lima FHB, Ticianelli EA. Oxygen reduction reaction on nanosized manganese oxide particles dispersed on carbon in alkaline solutions. Journal of Power Sources 2006;158:735–9.
- [106] Tseung ACC, Hobbs BS. Influence of oxygen partial pressure on the electrocatalytic activity of nickel-oxide oxygen electrodes. Electrochimica Acta 1972;17:1557–62.
- [107] Ponce J, Rehspringer JL, Poillerat G, Gautier JL. Electrochemical study of nickelaluminium-manganese spinel Ni<sub>x</sub>Al<sub>1-x</sub>Mn<sub>2</sub>O<sub>4</sub>. Electrocatalytical properties for the oxygen evolution reaction and oxygen reduction reaction in alkaline media. Electrochimica Acta 2001;46:3373–80.
- [108] Restovic A, Rios E, Barbato S, Ortiz J, Gautier JL. Oxygen reduction in alkaline medium at thin  $Mn_xCo_3-xO_4$  ( $0 \le x \le 1$ ) spinel films prepared by spray pyrolysis. Effect of oxide cation composition on the reaction kinetics. Journal of Electroanalytical Chemistry 2002;522:141–51.
- [109] Ríos E, Abarca S, Daccarett P, Nguyen Cong H, Martel D, Marco JF, et al. Electrocatalysis of oxygen reduction on  $Cu_xMn_3-xO_4$  (1.0  $\leq x \leq$  1.4) spinel particles/polypyrrole composite electrodes. International Journal of Hydrogen Energy 2008;33:4945–54.

- [110] Tulloch J, Donne SW. Activity of perovskite La<sub>1-x</sub>Sr<sub>x</sub>MnO<sub>3</sub> catalysts towards oxygen reduction in alkaline electrolytes. Journal of Power Sources 2009:188:359–66.
- [111] Wang G, Bao Y, Tian Y, Xia J, Cao D. Electrocatalytic activity of perovskite  $La_{1-x}Sr_xMnO_3$  towards hydrogen peroxide reduction in alkaline medium. Journal of Power Sources 2010;195:6463–7.
- [112] Kiros Y, Schwartz S. Pyrolyzed macrocycles on high surface area carbons for the reduction of oxygen in alkaline fuel cells. Journal of Power Sources 1991:36:547–55.
- [113] Kivisaari J, Lamminen J, Lampinen MJ, Viitanen M. Preparation and measurement of air electrodes for alkaline fuel cells. Journal of Power Sources 1990;32:233-41.
- [114] Khomenko VG, Barsukov VZ, Katashinskii AS. The catalytic activity of conducting polymers toward oxygen reduction. Electrochimica Acta 2005;50:1675–83.
- [115] Tomantschger K, McClusky F, Oporto L, Reid A, Kordesch K. Development of low cost alkaline fuel cells. Journal of Power Sources 1986;18:317–35.
- [116] Huang H, Zhang W, Li M, Gan Y, Chen J, Kuang Y. Carbon nanotubes as a secondary support of a catalyst layer in a gas diffusion electrode for metal air batteries. Journal of Colloid and Interface Science 2005;284:593–9.
- [117] Zhuk AZ, Sheindlin AE, Kleymenov BV, Shkolnikov EI, Lopatin MY. Use of low-cost aluminum in electric energy production. Journal of Power Sources 2006;157:921–6.
- [118] Mance A, Cerović D, Mihajlović A. The effect of gallium and phosphorus on the corrosion behaviour of aluminium in sodium chloride solution. Journal of Applied Electrochemistry 1985;15:415–20.
- [119] Doche ML, Novel-Cattin F, Durand R, Rameau JJ. Characterization of different grades of aluminum anodes for aluminum/air batteries. Journal of Power Sources 1997;65:197–205.
- [120] Yang S, Knickle H. Design and analysis of aluminum/air battery system for electric vehicles. Journal of Power Sources 2002;112:162–73.
- [121] Zaromb S. The use and behavior of aluminum anodes in alkaline primary batteries. Journal of The Electrochemical Society 1962;109:1125–30.
- [122] Keir DS, Pryor MJ, Sperry PR. Galvanic corrosion characteristics of aluminum alloyed with group IV metals. Journal of The Electrochemical Society 1967:114:777–82.
- [123] Keir DS, Pryor MJ, Sperry PR. The influence of ternary alloying additions on the galvanic behavior of aluminum-tin alloys. Journal of The Electrochemical Society 1969;116:319–22.
- [124] Tuck CDS, Hunter JA, Scamans GM. The electrochemical behavior of Al-Ga alloys in alkaline and neutral electrolytes. Journal of The Electrochemical Society 1987;134:2970–81.
- [125] Macdonald DD, Real S, Urquidi-Macdonald M. Evaluation of alloy anodes for aluminum-air batteries. Journal of The Electrochemical Society 1988;135:2397-409.
- [126] Venugopal A, Raja VS. The self regulating nature of In on the potential of Al in 3.5% NaCl solution. Corrosion Science 1997:39:1285–9.
- [127] Barbucci A, Cerisola G, Bruzzone G, Saccone A. Activation of aluminium anodes by the presence of intermetallic compounds. Electrochimica Acta 1997;42:2369–80.
- [128] Gudic S, Radosevic J, Smoljko I, Kliskic M. Cathodic breakdown of anodic oxide film on Al and Al–Sn alloys in NaCl solution. Electrochimica Acta 2005;50:5624–32.
- [129] Kliskic M, Radosevic J, Gudic S. Yield of hydrogen during cathodic polarisation of Al–Sn alloys. Electrochimica Acta 2003;48:4167–74.
- [130] Gudic S, Smoljko I, Kliskic M. Electrochemical behaviour of aluminium alloys containing indium and tin in NaCl solution. Materials Chemistry and Physics 2010;121:561–6.
- [131] Tang Y, Lu L, Roesky HW, Wang L, Huang B. The effect of zinc on the aluminum anode of the aluminum-air battery. Journal of Power Sources 2004;138:313–8.
- [132] Kapali V, Venkatakrishna Iyer S, Balaramachandran V, Sarangapani KB, Ganesan M, Anbu Kulandainathan M, et al. Studies on the best alkaline electrolyte for aluminium/air batteries. Journal of Power Sources 1992;39:263–9.
- [133] Mance A, Cerović D, Mihajlović A. The effect of small additions of indium and thallium on the corrosion behaviour of aluminium in sea water. Journal of Applied Electrochemistry 1984;14:459–66.
- [134] Flamini D, Saidman S. Polarisation behaviour of Al-Zn-Ga alloy in chloride medium. Journal of Applied Electrochemistry 2008;38:663-8.
- [135] Saidman SB, Garcia SG, Bessone JB. Electrochemical behaviour of Al-In alloys in chloride solutions. Journal of Applied Electrochemistry 1995;25:252-8.
- [136] Nestoridi M, Pletcher D, Wood RJK, Wang S, Jones RL, Stokes KR, et al. The study of aluminium anodes for high power density Al/air batteries with brine electrolytes. Journal of Power Sources 2008;178:445–55.
- [137] Nestoridi M, Pletcher D, Wharton JA, Wood RJK. Further studies of the anodic dissolution in sodium chloride electrolyte of aluminium alloys containing tin and gallium. Journal of Power Sources 2009;193:895–8.
- [138] El Abedin S, Saleh AO. Characterization of some aluminium alloys for application as anodes in alkaline batteries. Journal of Applied Electrochemistry 2004;34:331–5.
- [139] Sarangapani KB, Balaramachandran V, Kapali V, Iyer SV, Potdar MG, Rajagopalan KS. Aluminium as anode in primary alkaline batteries. Influence of additives on the corrosion and anodic behaviour of 2S aluminium in alkaline citrate solution. Journal of Applied Electrochemistry 1984;14:475–80.
- [140] Albert IJ, Kulandainathan MA, Ganesan M, Kapali V. Characterisation of different grades of commercially pure aluminium as prospective galvanic anodes

- in saline and alkaline battery electrolyte. Journal of Applied Electrochemistry 1989:19:547-51
- [141] Paramasivam M, Suresh G, Muthuramalingam B, Venkatakrishna Iyer S, Kapali V. Different commercial grades of aluminium as galvanic anodes in alkaline zincate solutions. Journal of Applied Electrochemistry 1991;21:
- [142] Wang XY, Wang JM, Shao HB, Zhang JQ, Cao CN. Influences of zinc oxide and an organic additive on the electrochemical behavior of pure aluminum in an alkaline solution. Journal of Applied Electrochemistry 2005;35:213-6.
- [143] Wang J-B, Wang J-M, Shao H-B, Zhang J-Q, Cao C-N. The corrosion and electrochemical behaviour of pure aluminium in alkaline methanol solutions. Journal of Applied Electrochemistry 2007;37:753-8.
- [144] Wang JB, Wang JM, Shao HB, Chang XT, Wang L, Zhang JQ, et al. The corrosion and electrochemical behavior of pure aluminum in additivecontaining alkaline methanol-water mixed solutions. Materials and Corrosion 2009;60:269-73.
- [145] Chang X, Wang J, Shao H, Wang J, Zeng X, Zhang J, et al. Corrosion and anodic behaviors of pure aluminum in a novel alkaline electrolyte. Acta Physico-Chimica Sinica 2008;24:1620-4.
- [146] Zeng XX, Wang JM, Wang QL, Kong DS, Shao HB, Zhang JQ, et al. The effects of surface treatment and stannate as an electrolyte additive on the corrosion and electrochemical performances of pure aluminum in an alkaline methanolwater solution. Materials Chemistry and Physics 2010;121:459-64.
- [147] Equey JF, Muller S, Desilvestro J, Haas O. Electrochemical properties of aluminum in weakly acidic sodium chloride solutions. Journal of The Electrochemical Society 1992;139:1499-502.
- [148] Breslin CB, Carroll WM. The electrochemical behaviour of aluminium activated by gallium in aqueous electrolytes. Corrosion Science 1992;33:1735-46.
- [149] Carroll WM, Breslin CB. Activation of aluminium in halide solutions containing activator ions. Corrosion Science 1992;33:1161-77.
- [150] Breslin CB, Carroll WM. The activation of aluminium by indium ions in chloride, bromide and iodide solutions. Corrosion Science 1993;34:327-41.
- [151] Saidman SB, Bessone JB. Activation of aluminium by indium ions in chloride solutions. Electrochimica Acta 1997;42:413–20.
- [152] Venugopal A, Raja VS. AC impedance study on the activation mechanism of aluminium by indium and zinc in 3.5% NaCl medium. Corrosion Science 1997;39:2053-65.
- [153] Sheindlin AE, Zhuk AZ, Shkolnikov EI, Vlaskin MS. Aluminum-hydrogen technologies for different applications. In: Russia-Taiwan Joint Symposium on Hydrogen & Fuel Cell Technologies. 2009.
- [154] Zhuk AZ, Kleymenov BV, Shkolnikov EI, Bersh AV, Grigor'yanc RR, Den'shikov KK, et al. Aluminum-hydrogen energy. Moscow: JIHT RAS; 2007 [in Russian].
- [155] Li Q, Bjerrum NJ. Aluminum as anode for energy storage and conversion: a review. Journal of Power Sources 2002;110:1–10.
- [156] Han B. Liang G. Neutral electrolyte aluminum-air battery with open configuration, Rare Metals 2006;25:360-3.
- Brindley GF. Composition of matter for generating hydrogen. US Patent; 1909.
- [158] Brindley GF, Bennie M. Composition of matter for manufacturing hydrogen gas, US Patent: 1909.
- [159] Rand DAJ, Woods R, Dell RM. Batteries for electric vehicles. Somerset: Research Studies Press Ltd: 1998.
- [160] Aleksandrov YA, Tsyganova EI, Pisarev AL. Reaction of aluminum with dilute aqueous NaOH solutions. Russian Journal of General Chemistry 2003;73:689-94.
- [161] Hiraki T, Yamauchi S, Iida M, Uesugi H, Akiyama T. Process for recycling waste aluminum with generation of high-pressure hydrogen. Environmental Science & Technology 2007;41:4454-7.
- [162] Martínez SS, López Benítes W, Álvarez Gallegos AA, Sebastián PJ. Recycling of aluminum to produce green energy. Solar Energy Materials and Solar Cells 2005:88:237-43.
- [163] Soler L, Candela AM, Macanás J, Muñoz M, Casado J. In situ generation of hydrogen from water by aluminum corrosion in solutions of sodium aluminate. Journal of Power Sources 2009;192:21-6.
- [164] Soler L, Macanas J, Munoz M, Casado J. Hydrogen generation from aluminum in a non-consumable potassium hydroxide solution. International Hydrogen Energy Congress and Exhibition IHEC 2005. Istanbul, Turkey; 2005.
- [165] Soler L, Macanás J, Muñoz M, Casado J. Aluminum and aluminum alloys as sources of hydrogen for fuel cell applications. Journal of Power Sources 2007:169:144-9.
- [166] Soler L, Macanás J, Muñoz M, Casado J. Synergistic hydrogen generation from aluminum, aluminum alloys and sodium borohydride in aqueous solutions. International Journal of Hydrogen Energy 2007;32:4702-10.
- [167] Stockburger D, Stannard JH, Rao BML, Kobasz W, Tuck CD. On-line hydrogen generation from aluminum in an alkaline solution. Hydrogen Storage Mater Batteries Electrochem; 1992. p. 431-44.
- [168] Soler L, Candela AM, Macanás J, Muñoz M, Casado J. Hydrogen generation by aluminum corrosion in seawater promoted by suspensions of aluminum hydroxide. International Journal of Hydrogen Energy 2009;34:8511-8.
- [169] Belitskus D. Reaction of aluminum with sodium hydroxide solution as a source of hydrogen. Journal of The Electrochemical Society 1970;117:1097-9.
- [170] Andersen ER. Renewable energy carrier system and method. US Patent; 2004.
- [171] Andersen ER, Andersen EJ. Method for producing hydrogen. US Patent; 2003.
- [172] Andersen ER, Andersen EJ. Apparatus for producing hydrogen. US Patent;
- [173] Checketts JH. Hydrogen generation pelletizaed fuel. US Patent; 1998.

- [174] Checketts JH. Hydrogen generation system and pelletized fuel. US Patent;
- [175] Gill GC. Hydrogen generator. US Patent; 1955.
- Hu H, Qiao M, Pei Y, Fan K, Li H, Zong B, et al. Kinetics of hydrogen evolution in alkali leaching of rapidly quenched Ni-Al alloy. Applied Catalysis A: General 2003;252:173-83.
- [177] Martínez SS, Albañil Sánchez L, Álvarez Gallegos AA, Sebastian PJ. Coupling a PEM fuel cell and the hydrogen generation from aluminum waste cans. International Journal of Hydrogen Energy 2007;32:3159-62.
- [178] Wang E-D, Shi P-F, Du C-Y, Wang X-R. A mini-type hydrogen generator from aluminum for proton exchange membrane fuel cells. Journal of Power Sources 2008;181:144-8.
- [179] Hiraki T, Akiyama T. Exergetic life cycle assessment of new waste aluminium treatment system with co-production of pressurized hydrogen and aluminium hydroxide. International Journal of Hydrogen Energy 2009:34:153-61.
- [180] Hiraki T, Takeuchi M, Hisa M, Akiyama T. Hydrogen production from waste aluminum at different temperatures with LCA. Materials Transactions 2005:46:1052-7.
- [181] Varshavskiy IL. Energy accumulation matters and their use. Kiev: Naukova Dumka; 1980 [in Russian].
- [182] Olivares-Ramírez JM, Castellanos RH, Marroquín de Jesús Á, Borja-Arco E, Pless RC. Design and development of a refrigeration system energized with hydrogen produced from scrap aluminum. International Journal of Hydrogen Energy 2008;33:2620-6.
- [183] Brooke AW, Bean JA, Bean RA. Metal-water fueled reactor for generating steam and hydrogen. US Patent; 1970.
- [184] Smith IE. Hydrogen generation by means of the aluminum/water reaction. Journal of Hydronautics 1972;6:106-9.
- [185] Kozin LF, Sokol'skiy DV, Sarmurzina RG, Podgorny AN, Varshavskiy IL, Nikitin AA, et al. Method of composition preparation. Russian Federation Patent;
- [186] Fan M-Q, Xu F, Sun L-X. Studies on hydrogen generation characteristics of hydrolysis of the ball milling Al-based materials in pure water. International Journal of Hydrogen Energy 2007;32:2809–15.
- [187] Kuech TF, Veuhoff E, Meyerson BS. Silicon doping of GaAs and  $Al_xGa_{1-x}As$ using disilane in metalorganic chemical vapor deposition. Journal of Crystal Growth 1984;68:48-53.
- [188] Shchurin VN, Baev AK, Tishevich VI. Zeolite modification with aluminum and efficiency of gas purification. Russian Journal of Applied Chemistry 2002:75:1252-5.
- [189] Shealy JR, Woodall JM. A new technique for gettering oxygen and moisture from gases used in semiconductor processing. Applied Physics Letters 1982:41:88-90
- [190] Kraychenko OV, Semenenko KN, Bulychev BM, Kalmykov KB, Activation of aluminum metal and its reaction with water. Journal of Alloys and Compounds 2005;397:58-62.
- [191] Parmuzina AV, Kravchenko OV. Activation of aluminium metal to evolve hydrogen from water. International Journal of Hydrogen Energy 2008:33:3073-6.
- [192] Ilyukhina AV, Kravchenko OV, Bulychev BM, Shkolnikov EI. Mechanochemical activation of aluminum with gallams for hydrogen evolution from water. International Journal of Hydrogen Energy 2010;35:1905-10.
- Goryunov YV, Pertsev NV, Summ BD. Rebinder effect. Moscow: Nauka; 1966.
- [194] Alinejad B, Mahmoodi K. A novel method for generating hydrogen by hydrolysis of highly activated aluminum nanoparticles in pure water. International Journal of Hydrogen Energy 2009;34:7934-8.
- [195] Fan M-q, Sun L-x, Xu F. Experiment assessment of hydrogen production from activated aluminum alloys in portable generator for fuel cell applications. Energy 2010;35:2922-6.
- [196] Mahmoodi K, Alinejad B. Enhancement of hydrogen generation rate in reaction of aluminum with water. International Journal of Hydrogen Energy 2010:35:5227-32.
- [197] Rosenband V, Gany A. Application of activated aluminum powder for generation of hydrogen from water. International Journal of Hydrogen Energy 2010:35:10898-904.
- [198] Yanilkin I, Shkol'nikov Y, Klyamkin S, Vlaskin M, Yanushko S, Tarasova S, et al. The combined system for fuel supply of fuel cells on the basis of the aluminum-water hydrogen generator and the metal hybride hydrogen storage. Thermal Engineering 2010;57:1112-8.
- [199] Shkolnikov E, Vlaskin M, Iljukhin A, Zhuk A, Sheindlin A. 2W power source based on air-hydrogen polymer electrolyte membrane fuel cells and water-aluminum hydrogen micro-generator. Journal of Power Sources 2008;185:967-72
- [200] Vlaskin MS, Shkolnikov EI, Zhuk AZ, Sheindlin AE. Aluminum and water as sources of energy and hydrogen. HFC-2009 Vancouver, Canada; 2009.
- [201] Uehara K, Takeshita H, Kotaka H. Hydrogen gas generation in the wet cutting of aluminum and its alloys. Journal of Materials Processing Technology 2002;127:174-7.
- Streletskii AN, Pivkina AN, Kolbanev IV, Borunova AB, Leipunskii IO, Pshechenkov PA, et al. Mechanical activation of aluminum. 2. Size, shape, and structure of particles. Colloid Journal 2004;66:736-44.
- [203] Ivanov YF, Osmonoliev MN, Sedoi VS, Arkhipov VA, Bondarchuk SS, Vorozhtsov AB, et al. Productions of ultra-fine powders and their use in high energetic compositions. Propellants, Explosives, Pyrotechnics 2003;28: 319-33.

- [204] Sarathi R, Sindhu TK, Chakravarthy SR. Generation of nano aluminium powder through wire explosion process and its characterization. Materials Characterization 2007;58:148–55.
- [205] Dong S, Zou G, Yang H. Thermal characteristic of ultrafine-grained aluminum produced by wire electrical explosion. Scripta Materialia 2001;44:17–23.
- [206] Gromov AA, Förter-Barth U, Teipel U. Aluminum nanopowders produced by electrical explosion of wires and passivated by non-inert coatings: characterisation and reactivity with air and water. Powder Technology 2006;164:111–5.
- [207] Inoue A, Kim BG, Nosaki K, Yamaguchi T, Masumoto T. Production of ultrafine aluminum and aluminum nitride particles by plasma—alloy reaction and their microstructure and morphology. Journal of Applied Physics 1992;71:4025–9.
- [208] Donaldson A, Cordes R. Rapid plasma quenching for the production of ultrafine metal and ceramic powders. JOM 2005;57:58–63.
- [209] Laha T, Agarwal A, McKechnie T, Rea K, Seal S. Synthesis of bulk nanostructured aluminum alloy component through vacuum plasma spray technique. Acta Materialia 2005;53:5429–38.
- [210] Chen L, Song W-I, Guo L-g, Xie C-s. Thermal property and microstructure of Al nanopowders produced by two evaporation routes. Transactions of Nonferrous Metals Society of China 2009;19:187–91.
- [211] Axelbaum RL, Lottes CR, Huertas JI, Rosen LJ. Gas-phase combustion synthesis of aluminum nitride powder. Symposium (International) on Combustion 1996;26:1891–7.
- [212] Barr J, Axelbaum R, Macias M. Processing salt-encapsulated tantalum nanoparticles for high purity, ultra high surface area applications. Journal of Nanoparticle Research 2006;8:11–22.
- [213] Calcote HF, Felder W. A new gas-phase combustion synthesis process for pure metals, alloys, and ceramics. Symposium (International) on Combustion 1992;24:1869–76.
- [214] Higa KT, Johnson CE, Hollins RA. Preparation of fine aluminum powders by solution methods. US Patent; 1999.
- [215] Gladfelter WL, Boyd DC, Jensen KF. Trimethylamine complexes of alane as precursors for the low-pressure chemical vapor deposition of aluminum. Chemistry of Materials 1989;1:339–43.
- [216] Kim D-H, Kim B-Y. Characteristics of aluminum films prepared by metalor-ganic chemical vapor deposition using dimethylethylamine alane on the plasma-pretreated TiN surfaces. Korean Journal of Chemical Engineering 2000;17:449–54.
- [217] Rat'ko Al, Romanenkov VE, Bolotnikova EV, Krupen'kina ZV. Hydrothermal synthesis of porous Al<sub>2</sub>O<sub>3</sub>/Al metal ceramics. I. Oxidation of aluminum powder and structure formation of porous Al(OH)<sub>3</sub>/Al composite. Kinetics and Catalysis 2004:45:141–8.
- [218] Tikhov S, Sadykov V, Ratko A, Kouznetsova T, Romanenkov V, Eremenko S. Kinetics of aluminum powder oxidation by water at 100 °C. Reaction Kinetics and Catalysis Letters 2007:92:83–8.
- [219] Wu HC, Ou HJ, Hsiao HC, Shih TS. Explosion characteristics of aluminum nanopowders. Aerosol and Air Quality Research 2010;10:38–42.
- [220] Gromov A, Il'in A, Foerter-Barth U, Teipel U. Effect of the passivating coating type, particle size, and storage time on oxidation and nitridation of aluminum powders. Combustion, Explosion, and Shock Waves 2006;42: 177–84.
- [221] Park K, Rai A, Zachariah M. Characterizing the coating and size-resolved oxidative stability of carbon-coated aluminum nanoparticles by single-particle mass-spectrometry. Journal of Nanoparticle Research 2006;8:455–64.
- [222] Kwon Y-S, Gromov AA, Ilyin AP, Rim G-H. Passivation process for superfine aluminum powders obtained by electrical explosion of wires. Applied Surface Science 2003;211:57–67.
- [223] Gopienko VG. Production of aluminum and aluminum alloy powders. Handbook of non-ferrous metal powders. Oxford: Elsevier; 2009. p. 265–83.

- [224] Farber M, Srivastava RD, Uy OM. Mass spectrometric determination of the thermodynamic properties of the vapour species from alumina. Journal of the Chemical Society, Faraday Transactions 1: Physical Chemistry in Condensed Phases 1972;68:249–58.
- [225] Guo J, Goodings JM, Hayhurst AN. What are the main gas-phase species formed by aluminum when added to a premixed flame? Combustion and Flame 2007;150:127–36.
- [226] Jensen DE, Jones GA. Flame-photometric determination of the standard enthalpies of formation of Al(OH)<sub>2</sub> and AlO. Journal of the Chemical Society, Faraday Transactions 1: Physical Chemistry in Condensed Phases 1972;68:259–68.
- [227] Washburn EB, Webb JA, Beckstead MW. The simulation of the combustion of micrometer-sized aluminum particles with oxygen and carbon dioxide. Combustion and Flame 2010;157:540–5.
- [228] Sheĭndlin A, Bityurin V, Zhuk A, Zalkind V, Ivanov P, Miroshnichenko V. Aluminum-hydrogen MHD electric-energy generators. Doklady Physics 2009;54:202-4.
- [229] Bityurin VA, Galaktionov AV, Kolpakov AV. Reducing radiative losses in aluminum-hydrogen MHD generators. Technical Physics Letters 2010;36: 1046–8.
- [230] Potapova YV, Tikhov SF, Sadykov VA, Fenelonov VB. Kinetics of aluminium powder oxidation by water vapor at moderate temperatures. Reaction Kinetics and Catalysis Letters 2001;73:55–61.
- [231] Vlaskin MS, Shkolnikov EI, Bersh AV. Oxidation kinetics of micron-sized aluminum powder in high-temperature boiling water. International Journal of Hydrogen Energy 2011;36:6484–95.
- [232] Bersh AV, Zhukov NN, Ivanov YuL, Ikonnikov VK, Mazalov YuA, Ryzhkin VYu, et al. Method of aluminum hydroxides and oxides and hydrogen production. Russian Federation Patent; 2004.
- [233] Mazalov YuA, Bersh AV, Ivanov YuL. Method of aluminum hydroxides and oxides and hydrogen production and the realization divice. Russian Federation Patent; 2005.
- [234] Nikiforov BV, Rubal'skiy DM, Sokolov VS, Chigarev AV, Davidov VN, Dmitriev AL, et al. Energy plant of submarine, Russian Federation Patent; 2004.
- [235] Vlaskin MS, Shkolnikov EI, Bersh AV, Zhuk AZ, Lisicyn AV, Sorokovikov AI, et al. An experimental aluminum-fueled power plant. Journal of Power Sources 2011;196:8828–35.
- [236] Vlaskin MS, Shkol'nikov El, Lisitsyn AV, Bersh AV. Thermodynamic calculation of the parameters of a reactor for oxidizing aluminum in wet saturated steam. Thermal Engineering 2010;57:794–801.
- [237] Vlaskin MS, Shkolnikov EI, Lisicyn AV, Bersh AV, Zhuk AZ. Computational and experimental investigation on thermodynamics of the reactor of aluminum oxidation in saturated wet steam. International Journal of Hydrogen Energy 2010:35-1888-94
- [238] Bersh AV, Lisitsyn AV, Sorokovikov AI, Vlaskin MS, Mazalov YA, Shkol'nikov EI. Study of the processes of steam-hydrogen mixture generation in a reactor for hydrothermal aluminum oxidation for power units. High Temperature 2010:48:866-73.
- [239] Franzoni F, Milani M, Montorsi L, Golovitchev V. Combined hydrogen production and power generation from aluminum combustion with water: analysis of the concept. International Journal of Hydrogen Energy 2010:35:1548–59.
- [240] Miller TF, Walter JL, Kiely DH. A next-generation AUV energy system based on aluminum-seawater combustion. In: Symposium on Autonomous Underwater Vehicle Technology. 2002. p. 111–9.
- [241] Franzoni F, Mercati S, Milani M, Montorsi L. Operating maps of a combined hydrogen production and power generation system based on aluminum combustion with water. International Journal of Hydrogen Energy 2011;36:2803–16.